

Fuel Turbopumps

CIL Item:

B200-18

. Component:

High Pressure Fuel Turbopump

Part Number:

RS007801

Failure Mode:

Loss of coolant flow to furbine inlet support struts and turbine bearing support bellows.

Prepared; Approved: D. Early T. Nguyen 4/21/99

Approval Date: Change #:

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Directive #; CCBD ME3-01-5206

Рапе:

		101
Phase	Failure / Effect Description	Criticality Hazard Reference
SMC 4 I	Possible failure of turbine bearing support bellows resulting in leakage from turbine inlet to discharge. Possible structural buckling of inlet support struts resulting in loss of concentricity with rotating parts and resultant turbine blade failure. Loss of vehicle.	1 ME-D15,M
	Redundancy Screens: SINGLE POINT FAILURE. N/A	ME-D1A,C
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#### SSME FMEA/CIL DESIGN

Component Group:

Fuel Turbopumps

CIL Item:

B200-18

Component:

High Pressive Fuel Turbopump

Parl Number:

R\$007501

Fallure Mode:

RESULTSUIT
Loss of coolant flow to turbine inlet support strute and turbine bearing support bellows.

Prepared: Approved:

D. Early T. Nguyen 4/21/89

Approval Date: Change #; Directiva #:

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Design / Document Reference

FAILURE CAUSE: A: Lift-off seal binding/ closure,

THE LIFT-OFF SEAL (1) IS A SPRING LOADED, PRESSURE ACTIVATED, FACE RIDING, CARBON NOSED SEAL. THE SCAL HOUSING AND PISTON RING ARE MANUFACTURED UTILIZING A-286 CRES BAR (2). A-286 CRES WAS SELECTED FOR ITS COMPRESSIVE STRENGTH, RESISTANCE TO HIGH PRESSURE HYDROGEN DEGRADATION, AND CRYOGENIC MECHANICAL PROPERTIES. THE MATERIAL IS SOLUTION THEATED AND AGE-HARDENED. THE SEAL PREVENTS HYDROGEN LEAKAGE INTO THE TURBINE OURNING PRESTART AND PROPELLANT DUMP. THE TURBOPUMP IS ASSEMBLED WITH A PRELOAD ON THE SFAL NOSE WHICH MATES WITH THE OUTSIDE DIAMETER LIP OF THE THIRD-STAGE SLEEVE (3). THE SEAL NOSE IS MANUFACTURED UTILIZING PSN CARBON WHICH WAS SELECTED FOR ITS SURFACE VELOCITY WEAR CHARACTERISTICS (2). THE PISTON RING IS DESIGNED TO PROVIDE AN INTERFERENCE FIT WITH THE OUTSIDE DIAMETER OF THE CARBON RING. HT424 EPOXY RESIN IS UTILIZED TO BOND THE CARBON RING IN THE PISTON. THE MATING UP OF THE THIRD-STAGE SLEEVE IS HARD CHROME PLATED AND POLISHED TO PROVIDE A SMOOTH AND WEAR RESISTANT SEALING SURFACE. BOTH THE SLEEVE MATING SURFACE AND THE LIFT-OFF SEAL NOSE ARE REQUIRED TO BE FLAT WITHIN 3 HELIUM LIGHTBANDS. THE SEAL PRELOAD IS SUPPLIED BY 55 MAIN SPRINGS MANUFACTURED UTILIZING 302 CRES WIRE (2). THIS MATERIAL WAS SELECTED FOR ITS MODULUS OF ELASTICITY AND DUCTILITY AT CRYOGENIC TEMPERATURES, AND ITS PROPERTIES ARE NOT DEGRADED IN A HYDROGEN ENVIRONMENT (2)

DURING START, A PRESSURE UNBALANCE DEVELOPS ACROSS THE SEAL TO OFFSET THE SPRING LOAD AND RETRACT THE SEAL ALLOWING HYDROGEN COOLANT TO ENTER THE TURBINE. THE SEAL REMAINS OPEN LINTI! THE PRESSURE DECAYS DURING ENGINE SHUTDOWN. THE SEAL RETRACTION IS ACCOMMODATED BY AN INTERNAL CAVITY, WHICH IS VENTED TO AMBIENT PRESSURE THROUGH AN EXTERNAL DRAIN LINE. THE CAVITY DRAIN LINE IS ELECTRO-DISCHARGE MACHINED THROUGH THE SEAL HOUSING, ELIMINATING THE NEED FOR PLUG WELDS, AND MATES WITH A PASSAGE AT THE MAIN HOUSING (4) INTERFACE. THE SEAL AT THIS LOCATION IS PROVIDED BY A PRESSURE-ASSISTED "DOUGHNUT" STATIC SEAL (5), WHICH SEATS IN A GROOVE ON THE SEAL HOUSING FLANGE. THE SEAL IS MANUFACTURED LITE IZING SILVER-PLATED A-286 CRES BAR. A-286 CRES WAS SELECTED FOR ITS COMPRESSIVE STRENGTH. RESISTANCE TO HIGH-PRESSURE HYDROGEN DEGRADATION, AND ITS MECHANICAL PROPERTIES AT CRYOGENIC TEMPERATURES. THE MATERIAL IS SOLUTION TREATED AND AGE HARDENED. THE SILVER-PLATING PERMITS CONFORMANCE OF THE SEAL TO MINOR PREGULARITIES IN THE MATING SURFACES. A WIRE RETAINER IS MANUFACTURED UTILIZING 302 CRESTIOLDS THE "DOUGHNUT" SEAL IN THE RECESS OF THE LIFT-OFF SEAL TO PREVENT DISLOGEMENT DURING HANDLING AND INSTALLATION. THE BOLT PATTERN OF THE LIFT-OFF SEAL AND MAIN HOUSING ARE NOW-SYMMETRICAL TO ASSURE PROPER ALIGNMENT OF THE DRAIN LINE PASSAGES. DESIGN ANALYSIS SHOWS THAT WITH THE WORST COMBINATION OF TOLERANCES, ADEQUATE SEAL COMPRESSION WOULD BE MAINTAINED OVER THE FULL RANGE OF POSSIBLE DEFLECTIONS. DRAIN LINE PRESSURE AND TEMPERATURE ARE MONITORED ON ALL GREEN RUNS, WHICH WOULD INDICATE ANY HOT-GAS LEAKAGE PAST THIS SEAL. THE STATIC SEAL IS A NON-SERIALZED PART WHICH IS NOT TIME HISTORY TRACKED, BUT HAS INFINITE ALLOWABLE LIFE (7).

THE INTERNAL CAVITY IS FORMED BY STEPPED DIAMETERS ON THE SEAL PISTON AND MATING DIAMETERS ON THE SEAL HOUSING. THE TWO SPRING-LOADED INTERNAL SEALS PROVIDE SEALING BETWEEN THE HIGH-PRESSURE HYDROGEN AND THE CAVITY DURING OPERATION. THE SEALS ARE MANUFACTURED UTILIZING VESPEL SP-211, WHICH WAS SELECTED FOR ITS SEALING AND LUBRICATING CHARACTERISTICS (2). THE SEALS ARE BOTTOMED AGAINST THE HOUSING UTILIZING WEDGE RINGS MANUFACTURED UTILIZING 303 CRES BAR. THE WEDGE RING PRELOAD IS SUPPLIED BY 36 SPRINGS MANUFACTURED UTILIZING 302 CRES WIRE. THE PUMP-END SPRINGS ARE BOTTOMED AGAINST A 302 CRES PLATE, WHICH IS SECURED BY A MATING GROOVE IN THE HOUSING. THE TURBINE-END SEAL SPRINGS ARE BOTTOMED AGAINST A 286 CRES PLATE, WHICH IS SECURED TO THE HOUSING UTILIZING TWELVE 300 SERIES CRES SCREWS. A 286 AND THE 300 SERIES CRES ALLOYS WERE SELECTED FOR THE SAME CHARACTERISTICS DISCUSSED ABOVE. THE SCREWS ARE STAKED AT THE SEAL ASSEMBLY TO PREVENT ROTATION. ASSEMBLY PROCEDURES FOR LOCKING DEVICES ENSURE DEFECT-PREE INSTALLATION (8). MOVEMENT OF THE SEAL PISTON IS GUIDED BY A BUSHING WHICH PILOTS IN A GROOVE IN THE SEAL HOUSING. THE BUSHING IS MANUFACTURED UTILIZING VESPEL SP-211, WHICH WAS SELECTED FOR ITS LUBRICATING CHARACTERISTICS (2). THE PISTON DIAMETERS WHICH MATE WITH THE VESPEL SEALS AND THE BUSHING ARE CHROME PLATED TO PROVIDE A SMOOTH SLIDING SURFACE. THE CAVITY DRAIN LINE IS SIZED TO ACCOMMODATE THE PREDICTED LEAKAGES WHICH WOULD RESULT FROM ONE SECONDARY SEAL MISSING.

THE LIFT-OFF SEAL HOUSING IS SECURED TO THE MAIN HOUSING BY 12 BOLTS (9) AND CUPWASHERS (10), WHICH ALSO ATTACH THE TURBINE HUB LABYRINTH SEAL (11) AND THE SECOND-STAGE AFT PLATFORM SEAL (12). THE LIFT OFF SEAL HOUSING OUTSIDE DIAMETER AND MAIN HOUSING INSIDE DIAMETER ARE CLOSELY TOLERANCED TO ASSURE ACCURATE PILOTING OF THE SEAL STACK AND MINIMIZE THE EFFECT OF HOUSING DEFLECTIONS ON THE SEAL INTERNAL CLEARANCES. GROOVES IN THE MAIN HOUSING AND TURBINE HUB LABYRINTH SEAL PILOT STATIC SEALS (13) AT THESE LOCATIONS. ANALYSIS REVEALS THE LIFT-OFF SEAL DESIGN ALONG WITH OPERATING CLEARANCES PRECLUDES A COMPLETE LIFT-OFF SEAL CLOSURE (14)

THE LIFT-OFF SEAL FUNCTIONAL OPERATION WAS DEMONSTRATED BY DESIGN VERIFICATION TESTS (15).

Fuel Turbopumps

CIL Item:

B200-18

Component:

High Pressure Fuel Turbopump

Parl Number: RS007501

Fallure Mode:

Loss of coolant flow to turbine inlet support struts and turbine bearing support bellows.

Prepared: Approved; Approvel Date:

D. Early T. Nguyen 4/21/99

Change #: Directive #:

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#### Design / Document Reference

(1) R0019230; (2) RSS 8580-10; (3) RS007501, RS007584; (4) RS007577, RS007568. (5) RES1116; (6) R0019234; (7) RL00532, CP320R0003B; (9) RL00351; (9) RS007595; (10) RS007523; (11) RS007553; (12) RS007593; (13) RD261-3016, RE1621; (14) IL SSME-0806; (15) RSS-404-111

FAILURE CAUSE: B: Coolant flow passage blockage.

HYDROGEN COOLANT IS SUPPLIED TO THE TURBINE BY FLOW PAST THE LOW-PRESSURE ORIFICE (1) OF THE BALANCE PISTON CAVITY AND PAST THE LIFT-OFF SEAL (2). A PORTION OF THE COOLANT ENTERS 8 HOLES ON THE HUB OF THE SECOND-STAGE TURBINE DISK (3) JUST UPSTREAM OF THE HUB LABYRINTH SEAL (4). THE FLOW CONTINUES DOWN THE CENTRAL CAVITY OF THE SECOND-STAGE DISK. A PORTION OF THIS COOLANT FLOWS THROUGH THE 16 HOLES IN THE ORIFICE RING (5) BETWEEN THE TURBINE DISKS. THIS FLOW IS SPLOT AND GUIDED BY THE TURBINE INTERSTAGE SEAL (6) TO COOL THE DOWNSTREAM SIDE OF THE FIRST-STAGE DISK (7) AND THE UPSTREAM SIDE OF THE SECOND-STAGE DISK. THE REMAINDER OF THE FLOW CONTINUES THROUGH THE FIRST-STAGE DISK AND COOLS THE TURBINE END BEARINGS (8). THIS FLOW IS THEN SPLIT AND GUIDED BY THE TURBINE BEARING SEAL (9). TO COOL THE UPSTREAM SIDE OF THE FIRST-STAGE DISK AND THE TURBINE END BEARINGS (8). THIS FLOW IS THEN SPLIT AND GUIDED BY THE TURBINE BEARING SUPPORT BODY THROUGH 4 HOLES AND THEN ENTERS THE BEARING SUPPORT BODY THROUGH 4 HOLES AND THEN ENTERS AN INTERNAL SHEET METAL MANIFOLD THROUGH 13 HOLES. THE COOLANT THEN IS DISTRIBUTED TO 3 HOLES IN LIFT-OFF SEAL FLOWS THROUGH THE LABYRINTH STEPS OF THE TURBINE HUB LABYRINTH SEAL PART OF THIS FLOW IS DIMERTED THROUGH 4 HOLES IN THE FLOW FROM THE OF THE FIRST-STEP. THE FLOW IS COLLECTED IN A MANIFOLD AND DISCHARGED THROUGH 3 HOLES IN THE FLOW IS DIMERTED THROUGH 12 HOLES IN THE LIFT-OFF SEAL AND MAIN HOUSING (12) TO ENTER THE COOLANT LINER. THE COOLANT CONTINUES THROUGH 3 HOLES IN EACH OF THE MAIN HOUSING STRUTS AND ENTERS A MANIFOLD AT THE DOWNSTREAM END OF THE TURBINE INNER RING IN THE LIFT-OFF SEAL HUB LABYRINTH SEAL INTERFACE BEFORE CONTINUING THROUGH 12 HOLES IN THE LIFT-OFF SEAL AND MAIN HOUSING STRUTS AND ENTERS A MANIFOLD AT THE DOWNSTREAM END OF THE TURBINE INNER RING IN THE TURBINE BEARING SUPPORT GOOLANT PASSAGES IN THE MOUNT RING AND THE TURBINE BEARING SUPPORT GOOLANT FLOW TO COOL THE BELLOWS. THE FLOW TO A MANIFOLD, WHERE IT DISCHARGES OUT 12 ORIFICES AND JOINS THE TURBINE BEARIN

THE REMAINDER OF THE COOLANT FLOW THROUGH THE TURBINE HUB LABYRINTH SEAL IS UTILIZED TO COOL THE DOWNSTREAM SIDE OF THE SECOND-STAGE DISK.

THE NUMBER OF PARALLEL PASSAGES FOR THE COCLANT FLOW, THE SIZE OF THE PASSAGES, AND THE QUANTITY OF THE FLOW MAKES THE TURBINE COCLANT CIRCUIT INSENSITIVE TO MINOR FLOW BLOCKAGE. THE PROPELLANT FILTER AT THE EXTERNAL TANK PRECLUDES CONTAMINANTS LARGE ENOUGH TO BLOCK THE PASSAGES (15). POST TEST/FLIGHT DRYING PURGES PREVENTS BLOCKAGE FROM ICE FORMATION RESULTING FROM ACCUMULATION OF MOISTURE BETWEEN HOT FIRES (16).

(1) R\$007559; (2) R0019230, (3) R\$007510; (4) R\$007553; (5) R\$007569; (6) R\$007592; (7) R\$007517; (8) R\$007502; (9) R\$007547; (10) R\$007524; (11) R\$007505; (12) R\$007577, R\$007588, (13) R\$007598; (14) R\$007599, (15) ICD 13M16000 (16) RL00059-04, OMR\$D V41CB0 050, OMR\$D V41CB0.080 (PHASE II), OMR\$D V41CB0 081 (PHASE III), OMR\$D V41CB0.083 (BLOCK I/IIA), OMR\$D V41CB0.083 (BLOCK I/IIIA)

FAILURE CAUSE: C: Failure of turbine bearing labyrinth seal.

THE TURBINE BEARING LABYRINTH SEAL (1) IS MANUFACTURED UTILIZING A HAYNES 188 FORGING, WHICH WAS SELECTED FOR ITS OXIDATION RESISTANCE, TENSILE STRENGTH AT ELEVATED TEMPERATURES AND LOW CYCLE FATIGUE LIFE IN A HIGH-PRESSURE HYDROGEN RICH STEAM ENVIRONMENT (2). THE MATERIAL IS ANNEALED TO IMPROVE MECHANICAL PROPERTIES. THE SEAL IS ATTACHED TO THE TURBINE SUPPORT (3) BY 8 BOLTS (4) LOCKED BY CUPVASHERS (5). TWO LABYRINTH STEPS CAUSE THE COOLANT FLOW TO DIMDE AS IT EXITS THE BEARINGS. PART OF THE FLOW IS ROUTED THROUGH THE TURBINE SUPPORT COOLANT CIRCUIT. THE REMAINDER PASSES THROUGH THE LABYRINTHS AND ALONG THE UPSTREAM FACE OF THE FIRST-STAGE DISK (6). THE SHAPE OF THE SEAL IS DESIGNED TO ROUTE THE COOLANT MORE EFFECTIVELY OVER THE DISKS, BOLTS (7). AND THE NUTS (8).

(1) RS007547, (2) RSS-8580-10; (3) RS007524; (4) RS007668; (5) RS007523; (6) RS007517, (7) RS007580; (8) RS007582

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CIL Item:

THE THEODERINGS B200-18

Component:

High Pressure Fuel Turbopump

Part Number:

RS007501

Fallure Mode:

Loss of coolant flow to turbine inlet support struts and turbine bearing support bellows.

Prepared: Approved: O. Early T. Nguyen 4/21/99

Approval Date: Change #:

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Design / Document Reference

FAILURE CAUSE: D: Failure of turbine hub laby rinth seal.

THE TURBINE HUB LABYRINTH SEAL (1) IS MANUFACTURED UTILIZING AN INCONEL 718 FORGING (2). THIS MATERIAL WAS SELECTED FOR ITS STRENGTH, RESISTANCE TO CORROSION AND STRESS CORROSION CRACKING, CRYOGENIC DUCTILITY, AND ITS INSENSITIVITY TO HYDROGEN ENVIRONMENT EMBRITTLEMENT IN ITS OPERATING ENVIRONMENT. THE MATERIAL IS SOLUTION TREATED AND AGE-HARDENED. THE SEAL HAS THREE STEPS, WITH EACH HAVING A SERIES OF TEETH. THE STEPS ALIGN WITH A SIM LAR SET OF STEPS ON THE HUB OF THE SECOND-STAGE CISK (2). THE SEAL IS CONFIGURED AT THE INNER DIAMETER TO DISTRIBUTE COOLANT FLOW TO THE TURBINE BEASINGS (4) AND TURBINE DISK/COOLANT LINER CIRCUITS. THE SEAL RESISTANCE DRIVES PART OF THE COOLANT FLOW FROM THE LIFT-OFF SEAL THROUGH B HOLES IN THE SECOND-STAGE DISK. THIS FLOW IS USED TO COOL THE TURBINE-END BEARINGS AND THE TURBINE DISKS (5). PART OF THE FLOW PASSING THROUGH THE LABYRINTH STEPS IS DIVERTED THROUGH 4 HOLES IN THE HUB SEAL BETWEEN THE FIRST AND SECOND LABYRINTH STEPS. THE FLOW IS ROUTED INTO THE HOUSING COCLANT LINER CIRCUITS THROUGH CHANNELS IN THE BUB LABYRINTH SEAL AND HOLES IN THE LIFT-OFF SEAL (6) FLANGE AND TURBOPUMP HOUSING (7). THE REMAINDER OF THE FLOW ENTERS THE CAVITY BETWEEN THE SEAL AND DISK. A LIP ON THE END OF THE HUB LABYRINTHS DIRECTS THE COOLANT AT THE HEADS OF THE DISK BOLTS (8) AND ACROSS THE FACE OF THE DISK. THE OUTSIDE DIAMETER OF THE HUS LABYRINTH SEAL PILOTS THE SECOND-STAGE AFT PLATFORM SEAL (9). A GROOVE IN THE HUS LABYRINTH SEAL FLANGE SERVES TO PILOT A STATIC SEAL (10) BETWEEN THE HUB LABYRINTH AND LIFT-OFF SEALS. THE HUB LABYRINTH SEAL IS SECURED TO THE TURBOPUMP THROUGH THE LIFT-OFF SEAL HOUSING BY 12 BOLTS (11) AND CUPWASHERS (12). STRETCH BOLTS ARE UTILIZED TO ASSURE THE REQUIRED CLAMPING LOAD AT ASSEMBLY IS APPLIED.

(1) RS007553; (2) RSS-8560-10; (3) RS007510; (4) RS007502; (5) RS007510 RS007517; (6) R0019230; (7) RS007577, RS007568; (8) RS007580; (9) RS007593, (10) RE1621; (11) R\$007595, (12) R\$007523

FAILURE CAUSE: E: Failure of vortex control paddle or its forque pin on end of shaft,

THE STUD (1) IS MANUFACTURED UTILIZING INCONEL 718 BAR. AN INCONEL 718 BAFFLE (1) IS THREADED TO THE TURRINE-END AND LOCKED WITH AN INCONEL 718 PIN (1) INCONEL 718 WAS SELECTED FOR ITS STRENGTH AND DUCTILITY AT CRYOGENIC TEMPERATURES AND ITS RESISTANCE TO CORROSION AND STRESS CORROSION CRACKING. IN THE CRYOGENIC ENVIRONMENT IT IS INSENSITIVE TO HYDROGEN ENVIRONMENT EMBRITTLEMENT (2). THE MATERIAL IS SOLUTION TREATED AND AGE-HARDENED. THE ANTI-VORTEX BAFFLE ASSURES ORDERLY FLOW OF THE COOLANT TO THE TURBINE-END BEARINGS AND DISKS.

(1) RS007514, R0019256; (2) RSS-8580-10

FAILURE CAUSE: F: Extensive failure of turbine bellows shield.

THE SHIELD (1) PROTECTS THE TURBINE BELLOWS (2) FROM HIGH TEMPERATURE TURBINE EXHAUST GAS. IT FORMS A CAVITY BETWEEN ITSELF AND THE TURBINE BELLOWS PERMITTING COOLANT FLOW ALONG THE OUTSIDE DIAMETER OF THE BELLOWS. THE BELLOWS SHIELD IS MANUFACTURED UTILIZING A HAYNES 188 FORGING. HAYNES 188 WAS SELECTED FOR ITS STRENGTH AT ELEVATED TEMPERATURES AND LOW CYCLE FATIGUE LIFE IN HIGH PRESSURE HYDROGEN (3). THE MATERIAL IS SHOT PEENED AND ANNEALED. THE SHIELD IS PILOTED BY ENGAGEMENT OF ITS UPSTREAM LIP BENEATH THE MAIN HOUSING HATBAND. SIX PEDESTALS AXIALLY BOTTOM THE SHIELD AGAINST THE TURBINE BEARING SUPPORT. FOUR STANDOFFS ON THE DOWNSTREAM LIP OF THE SHIELD PERMITS THE COOLANT TO DISCHARGE INTO THE TURBINE EXHAUST.

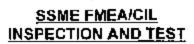
(1) RS007599; (2) RS007505, RS007524; (3) RSS-8580-10

FAILURE CAUSE: ALL CAUSES

THE HIGH AND LOW CYCLE FATIGUE LIFE FOR THE LIFT-OFF SEAL, TURBINE BEARING SEAL, TURDINE HUB LABYRINTH SEAL, VORTEX CONTROL PADDLE AND PIN, AND TURBINE BELLOWS SHIELD MEET CEI REQUIREMENTS (1). THE MINIMUM FACTORS OF SAFETY FOR THESE PARTS MEET CEI REQUIREMENTS (2). THE HARDWARE PARENT MATERIALS WERE CLEARED FOR FRACTURE MECHANICS/ADE FLAW GROWTH SINCE THEY CONTAIN NO FRACTURE CRITICAL PARTS, EXCEPT FOR THE FIRST AND SECOND-STAGE DISKS WHICH WERE CLEARED BY CRITICAL INITIAL FLAW SIZE DETECTABILITY (3). THE FMEA/CIL WELDS ARE CLEARED FOR FRACTURE MECHANICS/NDE FLAW GROWTH BY THE WELD ASSESSMENT (4). TABLE 8200 LISTS ALL FMEA/CIL WELDS AND IDENTIFIES THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE AND THOSE WELDS IN WHICH THE ROOT SIDE IS NOT ACCESSIBLE FOR INSPECTION. THOSE WELDS IN WHICH THE CRITICAL INITIAL FLAW SIZE IS NOT DETECTABLE ARE ACCEPTABLE FOR FLIGHT BY RISK ASSESSMENT (4) REUSE OF PARTS DURING OVERHAUL IS CONTROLLED BY THE REQUIREMENTS OF THE OVERHAUL SPECIFICATION (5).

(1) RL00532, CP320R0003B; (2) RSS-8548-16 CP320R0003B (3) NASA TASK 117; (4) RSS-8756; (6) RL00528





Fuel Turbopumps

CIL item:

B200-18

Component:

High Pressure Fuel Turbopump

Part Number:

RS007501

Failure Mode:

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Loss of coolant flow to turbine infel support struts and turbine bearing support bellows.

Prepared; Approved:

D. Early

Approval Date: Change #: Directive #:

T. Nguyen 4/21/99

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	rage: 1 or 4								
	Document Reference								
MATERIAL INTEGRITY IS VERIFIED PER DRAWING AND SPECIFICATION REQUIREMENTS									
UIREMENTS	R0019230 RA1103-001								
PER DRAWING REQUIREMENTS.	R0019230 RA1106-005								
EMENTS.	R0019230								
THE TENSILE STRENGTH IS VERIFIED PER DRAWING REQUIREMENTS.									
SPRING CLOSED ENDS ARE GROUND SQUARE AND DEBURRED PER DRAWING REQUIREMENTS.									
EQUIREMENTS PER WELD CLASS. DIOGRAPHIC, ULTRASONIC, AND	RL10011 RA0607-094 RA0115-116 RA0115-008 RA1115-001 RA0115-127								
QUIREMENT\$.	RA1609-002 RL00528								
rs.	R0019230								
UIREMENTS	RU10001								
AWING AND SPECIFICATION	R0D19230 R100505 R100505 R100605								
ON REQUIREMENTS .	RL00807								
REQUIREMENTS	R0019230 RA1618-005								
R SPECIFICATION	RL00352								
	RS007501								
	RE00351								
	DIREMENTS  ER DRAWING REQUIREMENTS.  EMENTS.  ER DRAWING REQUIREMENTS.  EQUIREMENTS PER WELD CLASS.  DIOGRAPHIC, ULTRASONIC, AND  QUIREMENTS.  S.  UIREMENTS.  AWING AND SPECIFICATION  ON REQUIREMENTS								

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FUCI Turnopumps

Component:

8200-18 High Pressure Fuel Turbopump RS007501

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	Failure Causes	Significant Characteristics	Page:	2 of 4
A		ASSEMBLY INTEGRITY	inspection(s) / Test(s) SEAL LEAK CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.	Document Reference
			TORQUE CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.	OMRSD V418Q0.010 OMRSD V418Q0.020 OMRSD V418Q0.050
В		HPF?P		OMRSD V418S0.020
		CLEANLINESS OF	COMPONENTS ADD VERIFIED OF EASTERN THE COMPONENTS ADD VERIFIED OF THE COMPONENT	RS007501
		COMPONENTS	COMPONENTS ARE VERIFIED CLEANED PER SPECIFICATION REQUIREMENTS.	RL10001
_		- ·· · · · · · · · · · · · · · · · ·	POST FLIGHT DRYING PURGES ARE PERFORMED PER SPECIFICATION REQUIREMENTS.	OMRSD V41C80 050 OMRSD V41C80 080 (PHASE II) OMRSD V41C80.081 (PHASE II) OMRSD V41C80.082 (BLOCK (/IIA) OMRSD V41C80 083 (BLOCK I/IA)
Γ.		SEAL. TURBINE BEARING DISK		<u> </u>
		MATERIAL INTEGRITY	MATERIAL INTEGRATY IS VERY OF SERVICE	RS007547 RS007517
			MATERIAL INTEGRITY IS VERIFIED PER SPECIFICATION REQUIREMENTS  FORGING IS REMETRANT AND LITERACOUNTS INTERPRETARIOR.	AMS 5772 RB0170-182
			FORGING IS PENETRANT AND ULTRASONIC INSPECTED PER SPECIFICATION REQUIREMENTS.	RA0115-118
		LOCELIA	SEAL IS PENETRANT INSPECTED PER SPECIFICATION REQUIREMENTS.	RA0115-012
		ASSEMBLY INTEGRITY	SEAL LABYRINTH AND DISK SEALING DIAMETERS ARE INSPECTED PER DRAWING REQUIREMENTS.	RA0115-116 RS007547
		HPFTP	THE ROTATING ASSEMBLY BALANCE IS VERIFIED PER SPECIFICATION REQUIREMENTS.	RS007517 RL00352
		ASSEMBLY INTEGRITY		RS007501
		HOGEWOLT INTEGRITY	TORQUE CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.	OMRSD V418S0.020
		· · · · · · · · · · · · · · · · · ·	TRAVEL CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.	, 141000.023
		SÉAL DISK		
		MATERIAL INTEGRITY	MATERIAL INTEGRITY IS A SERVICE AND A SERVIC	R\$007553 R\$007510
			MATERIAL INTEGRITY IS VERIFIED PER DRAWING AND SPECIFICATION REQUIREMENTS.  THE SEAL AND DISK ARE DRAWING AND SPECIFICATION REQUIREMENTS.	R\$007510 RB0170-153
		HEAT TREAT	THE SEAR AND DISK ARE PENGINANT INSPECTED PER SPECIFICATION REQUIREMENTS	RA0115-116
		Control of the Park	HEAT TREAT IS VERIFIED PER SPECIFICATION REQUIREMENTS	RA0611-020

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Component Group; CIL Item:

Fuel Turbapumps B200-18

Component:

High Pressure Fuel Turbopump RS007501

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Prepared: Approved: Approval Date:

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Failure Causes	Significant Characteristics	Inspection(s) / Test(s)	Document Reference				
ח	SURFACE FINISH	THE SEALING SURFACE IS VERIFIED PER DRAWING AND SPECIFICATION REQUIREMENTS.	R\$007510 RF0004-027				
	ASSEMBLY INTEGRITY	THE SEAL AND DISK DIAMETERS ARE VERIFIED PER DRAWING REQUIREMENTS	RS007553 RS007510				
		THE ROTATING ASSEMBLY BALANCE IS VERIFIED PER SPECIFICATION REQUIREMENTS.	RL00352				
	HPFTP		R\$007501				
	ASSEMBLY INTEGRITY	TORQUE CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.	OMRSD V41850.020				
		TRAVEL CHECKS ARE PERFORMED PRIOR TO EACH FLIGHT.					
!	BAFFLE, HPFTP PIN	<del></del>	R0019256 R5007514				
	MATERIAL INTEGRITY	MATERIAL INTEGRITY IS VERIFIED PER DRAWING AND SPECIFICATION REQUIREMENTS.	RS007514 RB0170-153				
		THE BAFFLE IS PENETRANT INSPECTED FOR SURFACE FLAWS BY PENETRANT INSPECTION PER SPECIFICATION REQUIREMENTS.	RA0115-116				
	HEAT TREAT HEAT TREAT IS VERIFIED PER SPECIFICATION REQUIREMENTS.						
	ASSEMBLY INTEGRITY	BAFFLE TORQUE IS VERIFIED PER DRAWING REOLIREMENTS.	RS007514				
		PIN STAKING IS VERIFIED PER ORAWING REQUIREMENTS.					
•	SHIELD		RS007599				
	MATERIAL INTEGRITY	MATERIAL INTEGRITY IS VERIFIED PER DRAWING REQUIREMENTS	170001233				
		FORGING IS PENETRANT AND ULTRASONIC INSPECTED PER SPECIFICATION REQUIREMENTS.	RA0115-116 RA0115-012				
		SHIELD IS PENETRANT INSPECTED PER SPECIFICATION REQUIREMENTS	RA0115-116				
	ASSEMBLY INTEGRITY	SHOT PEENING IS VERIFIED PER DRAWING REQUIREMENTS	RS007599				
		PASSIVATION IS VERIFIED PER SPECIFICATION REQUIREMENTS.	RA0110-018				
	HPFTP	·	RS007501				
	ASSEMBLY INTEGRITY	AN INTERNAL BORESCOPE INSPECTION IS PERFORMED PRIOR TO EACH FLIGHT.	OMRSD V418U0.075				
		SHIELD IS PENETRANT INSPECTED PER SPECIFICATION REQUIREMENTS	CMRSD V418U0.060				
LL CAUSES	HPFTP		RS007501				
	CLEANLINESS OF COMPONENTS	COMPONENTS ARE VERIFIED CLEANED PER SPECIFICATION REQUIREMENTS.	RL10001				
	ASSEMBLY INTEGRITY	OPERATION/PERFORMANCE IS VERIFIED BY ENGINE HOT-FIRE TESTING AND 2ND E $\&$ M TESTS ON INSPECTIONS	RL00050-04 RL00056-08				

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6200-18

Component:

High Pressure Fuel Turbopump

Part Number:

RS007501

Failure Mode:

Loss of coolant flow to turbine infet support struts and turbine bearing support bellows.

Prepared: Approved: Approval Date: D. Early T. Nguyen 4/21/99

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			rage;	4014
	Failure Causes	Significant Characteristics	Inspection(s) / Test(s)	Document Reference
•	, ALL CAUSES ASSEMBLY INTEGRITY		THE PUMP SUBASSEMBLIES ARE INSPECTED DURING OVERHAUL PER SPECIFICATION REQUIREMENTS, INSPECTIONS INCLUDE: VISUAL, DIMENSIONAL, PENETRANT, AND REPLACEMENT OF USAGE ITEMS AS APPLICABLE, PER OVERHAUL CLASSIFICATION.	RL00528 RA0115-116
			DATA FROM PREVIOUS FLIGHT OR HOT-FIRE IS REVIEWED FOR PROPER TURBOPUMP OPERATION/PERFORMANCE. (LAST TEST)	MSFC PLN 1228

Failure History:

Comprehensive failure history data is maintained in the Problem Reporting database (PRAMS/PRACA)

Reference: NASA letter SA21/88/308 and Rockeldyne letter 88RC09761

Coerational Use: Not Applicable.

8 128

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### SSME FMEAICIL FIELD CONFIGURATION VARIANCES FROM CIL RATIONALE

Component Group:

Fuel Turbopumps

Item Name:

High Pressure Fuel Turbonump

Hem Number: Part Number: B200 RS007501 Prepared: Approved: D. Early T. Nguyen 4/21/99

Approval Date: Change #: Directive #:

CCBD MET-01-ETOR

		Directive #;	CCBD ME3-01-5208	
Base Line Rationale	Veriance	Page:	1 of 2	
1. H200-15 RS007502; CAUSE A.		Change Rationale	Variani Dash Numbe	
B200-24; RS007605; CAUSE A B200-24; RS007605; CAUSE A THE INNER AND OUTER BEARING RACES ARE EDDY CURRENT INSPECTED PER RL00743.	BEARING RACES RECEIVED FROM SUPPLIER SPLIT BALL BEARING INCORPORATED RECEIVED NO GENERAL EDDY CURRENT INSPECTION	GENERAL EDDY CURRENT INSPECTION OF RACES REPLACES TYPE IVC IN PENETRANT INSPECTION IN DETECTING SURFACE FLAWS USE AS IS RATIONALE:  1. RACES SUPPLIED BY SPLIT BALL BEARING INCORPORATED RECEIVED 10X VISUAL AND TYPE IVC PENETRANT INSPECTION INSTEAD OF GENERAL EDDY CURRENT INSPECTION. FLAW OFFECTABILITY RELIABILITY LEVELS RETWEEN PENETRANT AND GENERAL EDDY CURRENT INSPECTIONS ARE 0.060 AND 0.057 RESPECTIVELY.		
2. B200-13 R5007527, RS007532, CAUSE A & B. B200-26; RS007532; CAUSE B. DIFFUSER HIDDEN SURFACES ARE PENETRANT INSPECTED PER RL00343,	SGME DIFFUSERS MAY NOT RECEIVE THE POST PROOF TEST HIDDEN SURFACE III PENETRANT INSPECTION	USE AS IS RATIONALE  1 IMPLEMENTATION OF HIDDEN SURFACE INSPECTION REQUIREMENT IS NOT A RESULT OF AN OBSERVED HARDWARE ANAQMALY BUT AS A RESULT OF ROCKETDYNE'S STAND DOWN.	SEE DAR 2751 FOR VARIANT PART SERIAL NUMBERS	
B200-14 CAUSE A, RS007568 B200-21 CAUSE B, RS007568 B200-26 CAUSE A, RS007568 WELD JOINTS RS007568 TABLE B200 HPF IP FMEA/CIL WELD BOINTS RS037568 HOUSING CURRENT CONFIGURATION IS BITE ONE(1) PIECE "-1121 CAP, USING FOUR (4) WELDS AND FOUR (4) WELD NUMBERS	SOME HOUSINGS (POSSIBLY TWO) MAY HAVE BEEN FABRICATED WITH THE TWO (2) PIECE *-113" CAPS (THIS HAS AN EXTRA WELD: #13 AND THREE FXTRA WELD NUMBERS 13, 58 69)	TO REDUCE CONFUSION ON THE DRAWING AND ON THE MANUFACTURING FLOOR	SEE MCR 2524. SAME -113 DASH NUMBER.	
B200-02: CAUSE A, R\$097524 CAUSE B, R\$007524; CAUSE C, R\$007524	SOME TURBINE BEARING SUPPORTS (RS007524) ARE FABRICATED USING A WSLDMENT OF HAYES 188 SHEET METAL INSTEAD OF THE EDM FORGING.	HIGH CYCLE FATIGUE INDUCED INLET SHEET METAL CRACKS OO OCCUR FROM THE CPERATIONAL ENVIRONMENT EXPERIENCED DURING ENGINE OPERATION. THE CRACKING IS CONTROLLED PER THE REQUIREMENTS:OF THE SHEET METAL INSPECTION SPECIFICATION (RL00655) WHICH LIMITS THE CRACKING LENGTH, SPACING, AND SHAPE, TO PRECLUDE SHEET METAL PIECES FROM DISLODGING. THE CRITERIA IS BASED ON CRACK GROWTH RATES AND ENGINE TEST EXPERIENCE. ANY CRACKS, WHICH EXCEED THE SPECIFICATION LIMITS, ARE WELD REPAIRED IRF0001-007). THE TURBINE BEARING SUPPORT WITH WELDED SHEET METAL IS LIFE LIMITED BY MAJOR WAIVER DAR 2709.	RS007524-201 AND SUBS.	

Component Group: Item Name:

Fuel Turbopumps High Pressure Fuel Turbopump B200

Item Number: Part Number:

RS007501

Prepared: Approved: Approvel Date: Change #: Oirective #:

D. Early T. Nguyen 4/21/99 2 CCBD ME3-01-5206

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Base Line Rationale	Variance	Change Rationale	Variant Dash Number
5 B200-16 CAUSE A, B200-17 CAUSE A, B200-18 CAUSE A, B200-19 CAUSE A, B200-22; CAUSE A,B,C,E	SOME LIFT-OFF SEAL HOUSING DRAIN LINES ARE FABRICATED USING INTERSECTING LINE DRILLED HOLES. THE HOLE THAT INTERSECTS THE OUTSIDE DIAMETER OF THE HOUSING FLANGE HAS A PLUG INSTALLED. THE PLUG IS THEN WELDED AT THE HOUSING OUTSIDE DIAMETER TO FORM A TIGHT GAS SEAL.	LOW CYCLE FATIGUE CRACKING HAS BEEN OBSERVED IN THE PLUG WELD, CRACK INITIATION AND PROPAGATION OCCURS AT SHUTDOWN/COOLDOWN ALL UNITS RECEIVE A STANDARD POST FLIGHT INSPECTIONS BY LEAK CHECK. LEAK CHECK POST FLIGHT WILL DETECT A CRACK PRIOR TO REFUGHT. POST LEAKAGE AT THE DRAIN LINE IS LIMITED TO 10 SCIM. ALL FLIGHT UNITS WILL CONTINUE TO RECEIVE A LEAK CHECK POST FLIGHT FOR THE DRAIN LINE PLUG WELD UNTIL THE ENTIRE FLEET IS RETROFIT WITH THE EDM DRAIN LINE CONFIGURATION	R0019230-071 AND SUBS.

# SSME FMEA/CIL WELD JOINTS

Companent Group:

Fuel Turbopumps

CIL Item:

Component: Parl Number: High Pressure Fuel Turbopump RS007501

Prepared: Approved: D. Early T. Nguyen 4/21/99

Approval Date: Change #: Directive #;

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Component	Basic Part Number	Wald Numbe	r Wald Tunn	Class	Root Side Not	Flaw 9	at Initial Size Not edable	
SIIIELO	R0012171	1.24, 29-52			Access	HCF		 Comments
SHIELD	R0012171	26	GTAW	(i	×			
LIFT-OFF SEAL	R0019230	1, 2	GTAW	li 				
SHIELD	R0019788	25. 26	GTAW	JI 	X			
SHIELD	R0019788	25. 26 27 50	GTAW	II				
SHIELD	R0019788		GTAW	1	×			
SHIFLD	R0019788	51, 52	GTAW	1				
BELLOWS	RS007505	53, 55	GTAW	4				
BELLOWS	RS007505	1-4	STAW	!		X		
NLET	RS007512	5, 6	E8W			X		
NLET	R\$007512	4 5-6	GTAW	1		X		
NLET	RS007512	5-6 7-10, 12, <b>13</b>	GTAW	1				
NLET	R\$007512	11	GTAW	'				
NLET	RS007512	14 15	EBW	li				
NLET	RS007512	16	GTAW GTAW					
FARING SUPPORT	RS00/524	14	EBW	,		Х		
EARING SUPPORT	RS007524	18	EBW/					
EARING SUPPORT	RS007524	29, 30	GTAW		×			
EARING SUPPORT	RS007524	1°8	GTAW		×	Х		
EARING SUPPORT	R\$007524	115, 121		1	×			
EARING SUPPORT	RS007524	120	E6M GTAM	I				
FARING SUPPORT	RS007524	229-241	GTAW	 	X			
OUSING	RS007568		GTAW	II	X			
	11500/308	75 223, 228 230 298	GTAW	1	х	х	х	· • •
DUSING	RS007568	14	GTAW	I				
DUSING	RS007568	48	EBW	1	x	x	×	
DUSING	RS0075EB	49	GTAW	1	x			
CUSING	RS007585	51	GTAW	ı	x	х		
DUSING	RSC07568	52	GTAW	0	x			
DUSING	PS007568	53	EBW	ï	^			
				•				

Component Group: CIL Item: Component: Part Number:

Fuel Turbopumps B200

High Prossure Fuel Turbopump RS007501

D. Early T. Nguyen 4/21/99

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Component	Basic Part Number	Weld Number	Meld Tuna	Class	Root Side Not Access	Flaw Det	af Initial Size Not ectable	
HOUSING	RS007668	55	<del></del>			ПСР	<u> </u>	Camments
HOUSING	R\$007568	56	EBW	11	X			_
HOUSING	RS007568	57, 324 325	WATE	II	X			
HOUSING	FIS007568	56 58	GTAW	JF 71				
HOUSING	RSD07568	59	GTAW EBW	II .	x	×	Х	
HOUSING	RS007568	74, 229, 297	GTAW	i				
IOUSING	RS007568	76, 77	GTAW	•	Х	х	Х	
HOUSING	RS007568	78-89	GTAW	'		X		
HOUSING	RS007568	90-101	GTAW	11	X			
IOUSING	RSQC75BB	102	GTAW	11	X			
OUSING	RS007588	139	GTAW	I  1	X			
HOUSING	R\$007558	140	GTAW	"	X			
HOUSING	RS007598	153, 154	GTAW	11	x x			
HOUSING	RS007568	174-185	GTAW	11	x			
HOUSING	RS007568	191 +92. 195, 196 245, 455 456	GTAW	ii	x	x		
HOUSING	RS/107568	193, 194, 197-202 204-207	GTAW	0 .		×		
HOUSING .	RS007568	203, 217, 218, 234, 236	GTAW	II	х	X		
IOUSING	R5007568		GTAW	II				
KONJSING	A\$007568	214 215	GTAW	I	×			1
CUSING	RS007568	222, 239	GTAW	Į.		x		
IOUSING	RS007568	224, 225	GTAW	ı		X	x	
OUSING	RS007568	226, 227	GTAW	1		x	.,	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
OUSING	RS007568	231, 232	GTAW .	II		x		
OUSING	RS007568	233	GTAW	l4	x			
OUSING	RS007568		GTAW	]				
OUSING	R\$007568		GTAW	η				
OUSING	R\$007568		GTAW	H.	x			
CUSING	RS007568		GTAW	il	x			
OUSING	RS007568		GTAW	ï		x	х	

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CIL Item:

Component: Part Number:

Fuel Turbopumps B200 High Pressure Fuel Turbopump RS007501

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Component	Projection bloombas		****		Root Flav Side Not De	ical Initial / Size Not rtectable	
Companent	Basic Part Number	Weld Number	Weld Type	Class	Access HCF	= LC <b>F</b>	Comments
HDU\$ING	RS007568	401-424	GTAW	ıı .	Х		
HOUSING	RS007568	425-448	GTAW 1	lì	х		
HOUSING	RS007568	450 (OPT)	GTAW	l:			
HOUSING	RS007568	450 (OPT)	€BW	JI	×		
HOUSING	RS007568	454	GTAW	Ħ	×		
HOUSING	R\$007568	537 (OPT)	GTAW	11			
ROTOR SEAL	RS207589	1	EBW	1			
SEA.	#IS007592	25	EB₩	Ц	х		